

NOTE: IF SUFFICIENT EDGE
ANGLE/BENT PLATE TO SPANDREL
BEAM/GIRDER 'OVERLAP' (do) IS
SPECIFIED, dc & de ARE NOT
ADDITIVE WHEN ESTABLISHING THE
EDGE OF SLAB/DECK TO EXTERIOR
WALL SYSTEM 'GAP' (dgap) — do
ACCOUNTS FOR dc & ELIMINATES dc
FROM CONCERN W/ RESPECT TO THE
EXTERIOR WALL SYSTEM.

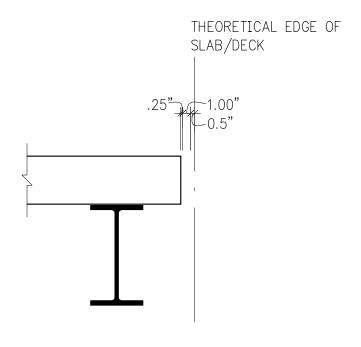
NOTES:

de = EDGE SPANDREL BEAM/GIRDER OR ANGLE/BENT PL SWEEP TOLERANCE

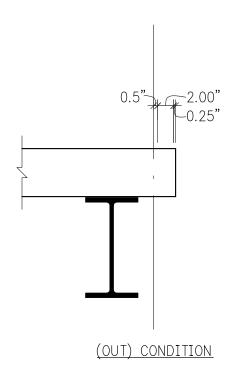


FIGURE 1.1 : STRUCTURAL STEEL TOLERANCES (dc & de ADDITIVE)





(IN) CONDITION



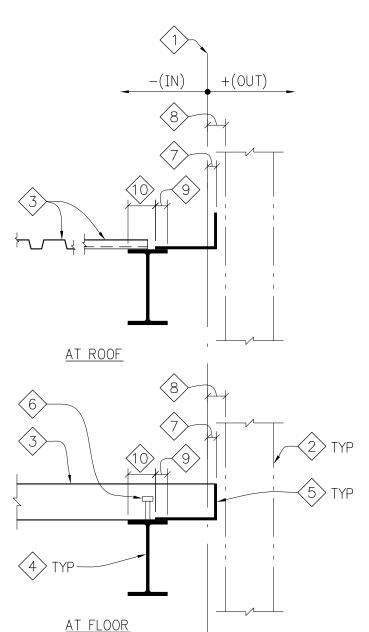
H = 100ftBAY = 40ft

NOTE: IF SUFFICIENT EDGE ANGLE/BENT PLATE TO SPANDREL BEAM/GIRDER 'OVERLAP' (do) IS SPECIFIED, dc & de ARE NOT ADDITIVE WHEN ESTABLISHING THE EDGE OF SLAB/DECK TO EXTERIOR WALL SYSTEM 'GAP' (dgap) — do ACCOUNTS FOR dc



FIGURE 1.2 : STRUCTURAL STEEL TOLERANCES (dc & de ADDITIVE)





- (1) THEORETICAL EDGE OF SLAB/DECK.
- 2 EXTERIOR WALL SYSTEM.
- 3 SLAB/DECK.
- 4 SPANDREL BEAM/GIRDER.
- 5 EDGE ANGLE/BENT PLATE, 1/4" THICK MINIMUM
- 6 HDAS (3/4"ø IS TYPICAL SIZE).
- SEE FIGURE 1.1 FOR +/- TOLERANCES.
 INCLUDES THE CUMULATIVE TOTAL
 CONSIDERING MILL, FABRICATION,
 & ERECTION PROCEDURES FOR COLUMN
 PLUMB 'dc' & EDGE SWEEP 'de'.
 COLUMN PLUMB EDGE SWEEP

 dc+ (OUT) de+ (OUT)
 dc- (IN) de- (IN)
- 8 EDGE OF SLAB/DECK TO INSIDE FACE
 OF EXTERIOR WALL SYSTEM SPECIFIED
 'GAP' REQUIRED: dgap = (ds+)+(dw-)
 WHERE: ds = de
 SEE FIGURE 1.3b FOR CHART.
 SEE EXTERIOR WALL SYSTEM FIGURES
 FOR 'dw' VALUES.
- SPECIFIED 'WIDTH' REQUIRED ON SPANDREL BEAM/GIRDER FLANGE TO ALLOW FOR SUFFICIENT 'OVERLAP' & SPACE FOR HDAS/DECK CONNECTIONS: df = do + dh
 WHERE: dh = SPACE REQUIRED ON SPANDREL BEAM/GIRDER FLANGE FOR HDAS/DECK.



FIGURE 1.3a: STRUCTURAL STEEL TOLERANCES

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HEIGHT	dc1 (in)		dc2 (in)		dc (in)		de (in)	
(ft)	-(IN)	+(OUT)	-(IN)	+(OUT)	-(IN)	+(OUT)	-(IN)	+(OUT)
10	0.25	0.25	0.24	0.24	0.49	0.49	0.5	0.5
20	0.25	0.25	0.48	0.48	0.73	0.73	0.5	0.5
30	0.25	0.25	0.72	0.72	0.97	0.97	0.5	0.5
40	0.25	0.25	0.96	0.96	1.21	1.21	0.5	0.5
50	0.25	0.25	1.00	1.20	1.25	1.45	0.5	0.5
60	0.25	0.25	1.00	1.44	1.25	1.69	0.5	0.5
70	0.25	0.25	1.00	1.68	1.25	1.93	0.5	0.5
80	0.25	0.25	1.00	1.92	1.25	2.17	0.5	0.5
90	0.25	0.25	1.00	2.00	1.25	2.25	0.5	0.5
100	0.25	0.25	1.00	2.00	1.25	2.25	0.5	0.5

NOTES: dc1 = COLUMN STARTING POINT TOLERANCE

dc2 = COLUMN PLUMB TOLERANCE

dc = dc1 + dc2 (dc1 = 0.125" SPECIFIED IN THE PROJECT

SPECIFICATIONS IN COMMON)

de = EDGE SPANDREL BEAM/GIRDER OR ANGLE/BENT PLATE SWEEP TOLERANCE (ASSUMING 40ft BAY WITH SPANDREL BEAM/GIRDER

FLANGE WIDTH 6" OR GREATER)

NOTE: IF SUFFICIENT EDGE ANGLE/BENT PLATE TO SPANDREL BEAM/GIRDER 'OVERLAP' (do) IS SPECIFIED, dc & de ARE NOT ADDITIVE WHEN ESTABLISHING THE EDGE OF SLAB/DECK TO EXTERIOR WALL SYSTEM 'GAP' (dgap) — do ACCOUNTS FOR dc & ELIMINATES dc FROM CONCERN W/ RESPECT TO THE EXTERIOR WALL SYSTEM.



FIGURE 1.3b : STRUCTURAL STEEL TOLERANCES



HEIGHT (ft)	dd (in)	do (in)	dh (in)	df (in)
10	1.00	1.49	2.00	3.49
20	1.00	1.73	2.00	3.73
30	1.00	1.97	2.00	3.97
40	1.00	2.21	2.00	4.21
50	1.00	2.45	2.00	4.45
60	1.00	2.69	2.00	4.69
70	1.00	2.93	2.00	4.93
80	1.00	3.17	2.00	5.17
90	1.00	3.25	2.00	5.25
100	1.00	3.25	2.00	5.25

NOTES: dd = RECOMMENDED DESIGN OVERLAP OF EDGE ANGLE/BENT PLATE TO SPANDREL BEAM/GIRDER

do = (dc+) + dd (SEE FIGURE 1.3b for dc+)

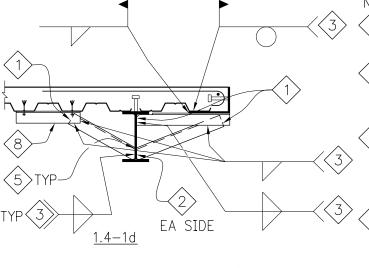
dh = SPACE REQUIRED ON SPANDREL BEAM/GIRDER FOR HDAS/DECK

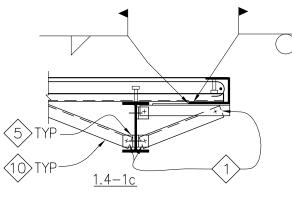
df = do + dh

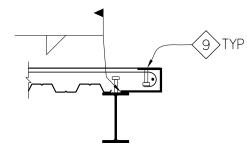


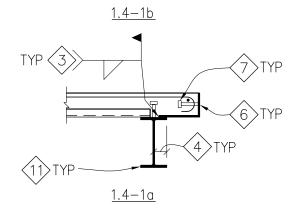
FIGURE 1.3c : STRUCTURAL STEEL TOLERANCES

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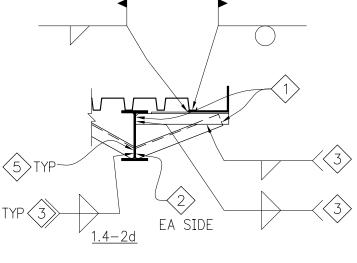


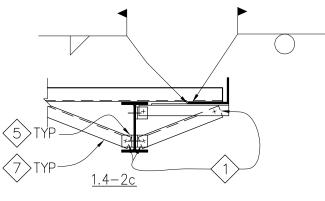
- 1) SQUARED ENDS OF PIECES FACILITATE EASE OF FABRICATION.
- 2 CONNECTION OF PIECES TO ONE SURFACE FACILITATES EASE OF FABRICATION AND/OR ERECTION.
- 3 DOWN OR SIDE WELDS IN LIEU OF OVERHEAD (FROM UNDERNEATH) WELDS FACILITATE EASE OF FABRICATION AND/OR ERECTION.
 - SUFFICIENT SPACE (SPANDREL BEAM/ GIRDER FLANGE WIDTH) MUST BE PROVIDED FOR CONNECTION OF HDAS/ DECK & ANGLE/BENT PLATE TO BEAM & SUFFICIENT 'OVERLAP' OF ANGLE/ BENT PLATE TO SPANDREL BEAM/GIRDER. SEE AISC SPECIFICATION FOR MINIMUM BEAM WEB THICKNESS REQUIRED TO ALLOW HDAS TO BE OFFSET FROM BEAM WEB.
- ALLOWANCE OF WELDED OR BOLTED CONNECTIONS ALLOW CUSTOMIZED FABRICATION EFFICIENCIES.
- ANGLES PROVIDE EASE OF FABRICATION
 IN LIEU OF BENT PLATES. GAGE METAL
 IS MORE COST EFFECTIVE THAN PLATE.
 PROVIDED BY STEEL FABRICATOR/ERECTOR.
- The House the House that the House the House the House the House t
- (8) CONNECTION OF KICKER PERPENDICULAR TO DECK SPAN VIA ANGLE, WT, OR BUILT-UP PLATE SECTION W/ ANCHORS INTO SLAB FACILITATES EASE OF FABRICATION & ERECTION OVER SKEWING KICKER TO BE WELDED TO ADJACENT BEAM. BY STEEL FABRICATOR/ERECTOR.
- 9 EMBED PLATE BY STEEL FABRICATOR.
- KICKERS BY STEEL FABRICATOR/ ERECTOR.
- 11) NO CAMBER OF THE SPANDREL BEAM/
 GIRDER IS PREFERRED (IF POSSIBLE)
 TO HELP CONTROL ISSUES OF FLOOR
 LEVELING AT THE BUILDING PERIMETER.

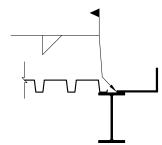


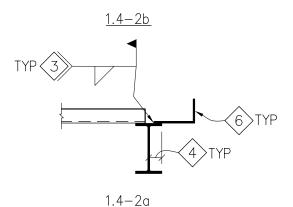
FIGURE 1.4-1 : STRUCTURAL STEEL CONSTRUCTION ISSUES - FLOOR









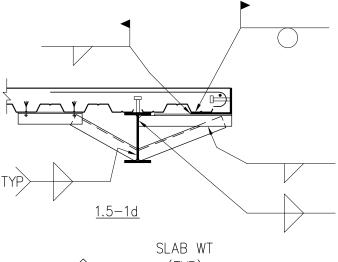


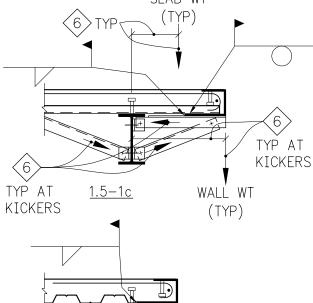
- SQUARED ENDS OF PIECES FACILITATE EASE OF FABRICATION.
- CONNECTION OF PIECES TO ONE SURFACE FACILITATES EASE OF FABRICATION AND/OR ERECTION.
- OVERHEAD (FROM UNDERNEATH) WELDS FACILITATE EASE OF FABRICATION AND/OR ERECTION.
- 4 SUFFICIENT SPACE (SPANDREL BEAM/ GIRDER FLANGE WIDTH) MUST BE PROVIDED FOR CONNECTION OF ANGLE/ BENT PLATE TO BEAM.
- ALLOWANCE OF WELDED OR BOLTED CONNECTIONS ALLOW CUSTOMIZED FABRICATION EFFICIENCIES.
- ANGLES PROVIDE EASE OF FABRICATION IN LIEU OF BENT PLATES. GAGE METAL IS MORE COST EFFECTIVE THAN PLATE. BY STEEL FABRICATOR/ERECTOR.
- 7 KICKERS BY STEEL FABRICATOR/ ERECTOR.



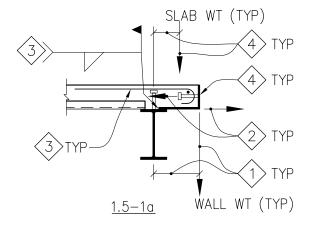
FIGURE 1.4-2 : STRUCTURAL STEEL CONSTRUCTION ISSUES - ROOF







1.5-1b

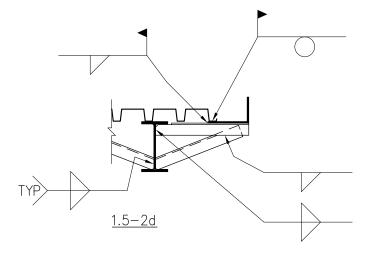


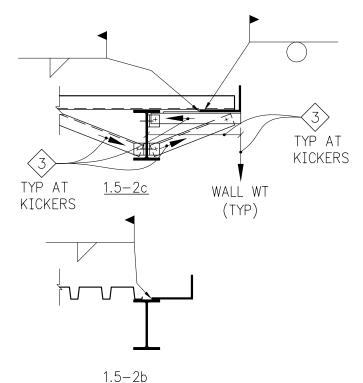
- SEE EXTERIOR WALL SYSTEM SKETCHES.
 EXTERIOR WALL SYSTEM DESIGNED FOR
 ECCENTRICITY FROM EXTERIOR WALL
 SYSTEM CENTER OF GRAVITY TO EDGE
 OF SLAB.
- FOR EXTERIOR WALL SYSTEM CONNECTIONS TO FACE OF EDGE OF SLAB: DESIGN ANGLE/BENT PLATE, HDAS/DAS, AND CONNECTIONS FOR EXTERIOR WALL SYSTEM WEIGHT APPLIED AT CORRESPONDING ECCENTRICITY TO EDGE OF SLAB.
- 3 DESIGN SLAB REINFORCING TO TAKE EXTERIOR WALL SYSTEM WEIGHT APPLIED AT CORRESPONDING ECCENTRICITY TO BEAM CENTERLINE.
- 4 DESIGN EDGE OF SLAB ANGLE/BENT PLATE & CONNECTIONS FOR SLAB WET CONCRETE WEIGHT APPLIED FROM CENTER OF MASS BEYOND THE BEAM FLANGE TO THE BEAM CENTERLINE.
- FOR EXTERIOR WALL SYSTEM
 CONNECTIONS TO EMBED PLATES IN
 TOP OF SLAB: DESIGN ANGLE/BENT
 PLATE, HDAS/DAS, AND CONNECTIONS
 FOR EXTERIOR WALL SYSTEM WEIGHT
 APPLIED AT CORRESPONDING
 ECCENTRICITY TO EDGE OF SLAB.
- 6 KICKERS AND CONNECTIONS DESIGNED FOR EXTERIOR WALL SYSTEM + SLAB WET CONCRETE WEIGHT APPLIED AT CORRESPONDING ECCENTRICITY TO BEAM CENTERLINE.

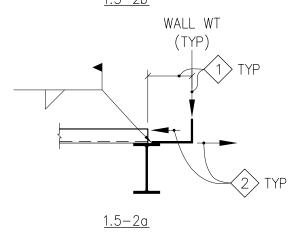


FIGURE 1.5-1 : STRUCTURAL STEEL ENGINEERING ISSUES - FLOOR







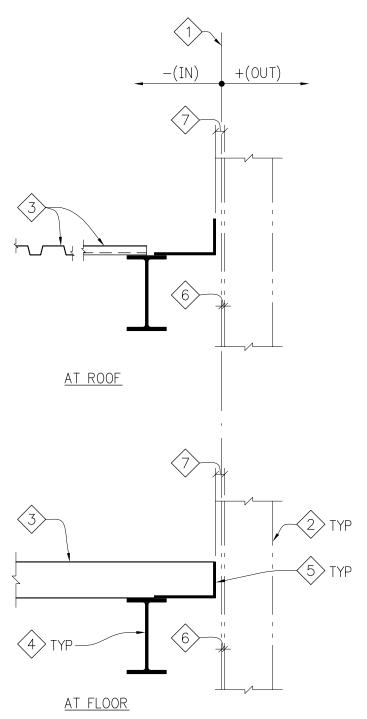


- 1) SEE EXTERIOR WALL SYSTEM SKETCHES. EXTERIOR WALL SYSTEM DESIGNED FOR ECCENTRICITY FROM EXTERIOR WALL STYSTEM CENTER OF GRAVITY TO EDGE OF DECK.
- DESIGN ANGLE/BENT PLATE,
 HDAS/DAS, AND CONNECTIONS FOR
 EXTERIOR WALL SYSTEM WEIGHT
 APPLIED AT CORRESPONDING
 ECCENTRICITY TO EDGE OF SLAB.
- KICKERS AND CONNECTIONS DESIGNED FOR EXTERIOR WALL SYSTEM WEIGHT APPLIED AT CORRESPONDING ECCENTRICITY TO BEAM CENTERLINE.



FIGURE 1.5-2 : STRUCTURAL STEEL ENGINEERING ISSUES - ROOF





- 1 THEORETICAL INSIDE FACE OF METAL STUD SYSTEM.
- 2 METAL STUD SYSTEM.
- 3 SLAB/DECK.
- 4 SPANDREL BEAM/GIRDER.
- 5 EDGE ANGLE/BENT PLATE.
- 6 METAL STUD SYSTEM ± TOLERANCE. SEE FIGURE 2.1b FOR CHART.
- TEDGE OF SLAB/DECK TO INSIDE FACE OF METAL STUD SYSTEM GAP 'dgap' REQUIRED:

 dgap = (ds+) + (dw-).
 SEE FIGURE 2.1b FOR CHART.



FIGURE 2.1a : METAL STUD TOLERANCES

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HEIGHT	ds (in)		dw (in)		dgap	е	
(ft)	-(IN)	+(OUT)	-(IN)	+(OUT)	(in)	(in)	
10	0.5	0.5	0.13	0.13	0.63	1.25 + c	
20	0.5	0.5	0.13	0.13	0.63	1.25 + c	
30	0.5	0.5	0.13	0.13	0.63	1.25 + c	
40	0.5	0.5	0.13	0.13	0.63	1.25 + c	
50	0.5	0.5	0.13	0.13	0.63	1.25 + c	
60	0.5	0.5	0.13	0.13	0.63	1.25 + c	
70	0.5	0.5	0.13	0.13	0.63	1.25 + c	
80	0.5	0.5	0.13	0.13	0.63	1.25 + c	
90	0.5	0.5	0.13	0.13	0.63	1.25 + c	
100	0.5	0.5	0.13	0.13	0.63	1.25 + c	

NOTES: ds = de (VALUES TAKEN FROM CHART IN FIGURE 1.3b)

dw = EXTERIOR WALL SYSTEM TOLERANCE

dgap = (ds+) + (dw-)

dgap = 0.75" IS COMMON SPECIFIED 'GAP'

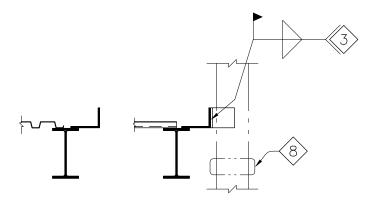
e = ds + dgap + c

SEE FIGURES 2.3 FOR GRAPHIC DEPICTION OF 'e' & 'c'

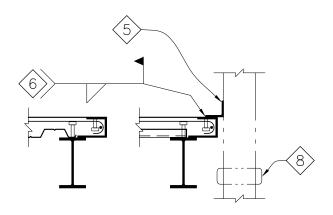




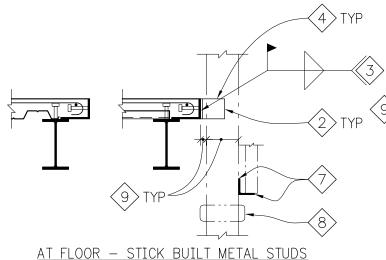
DASS CA



AT ROOF



AT FLOOR - PANELIZED METAL STUDS

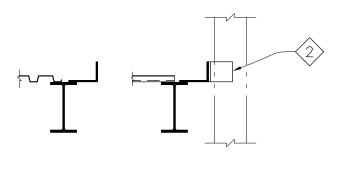


- SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.
- 2 METAL STUD CLIP BY METAL STUD SUPPLIER. CLIP IS EITHER DESIGNED TO DELIVER THE WALL WEIGHT TO THE EDGE ANGLE/BENT PLATE OR IS DESIGNED TO SLIP VERTICALLY.
- 3 CLIP EITHER FIELD WELDED OR SCREW /ANCHOR FASTENED TO EDGE ANGLE/BENT PLATE BY METAL STUD WALL SUPPLIER.
- 4 CLIP/SUPPORT ANGLE TO METAL STUD BY METAL STUD SUPPLIER.
- 5 CONTINUOUS STRONGBACK ANGLE SUPPLIED BY STEEL FABRICATOR & INSTALLED BY METAL STUD SUPPLIER.
- 6 SUPPORT STRONGBACK ANGLE TO SLAB/FRAME BY METAL STUD SUPPLIER.
- BRICK LEDGER ANGLES ARE SUPPLIED BY STEEL FABRICATOR. STEEL ERECTORS PREFER NOT TO HAVE TO FIELD WELDING TO METAL STUDS INCLUDED IN THEIR SCOPE.
 - CAPABILITY FOR ALLOWING VERTICAL SLIP IN THE METAL STUD WALL SYSTEM AT SOME LOCATION BETWEEN FLOORS IS REQUIRED TO ENSURE THAT RELATIVE DEFLECTIONS OF FLOORS/ROOF DO NOT LOAD/CRUSH METAL STUD WALL SYSTEM.
 - DEPENDING ON THE GOVERNING
 JURISDICTION, FIRE-SAFING MAY BE
 REQUIRED FROM THE OUTSIDE FACE
 OF ANGLE/BENT PLATE TO THE INSIDE
 OR OUTSIDE FACE OF METAL STUD
 WALL SYSTEM.



FIGURE 2.2-1 : METAL STUD CONSTRUCTION ISSUES - CASE A: BALLOON FRAMING





AT ROOF



- SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.
- 2 SEE FIGURE 2.2-1 FOR NOTES.
- METAL STUD SCREW/ANCHOR FASTENED TO SLAB BY METAL STUD SUPPLIER.
- CAPABILITY FOR ALLOWING
 VERTICAL SLIP IN THE METAL STUD
 WALL SYSTEM IS REQUIRED TO ENSURE
 THAT RELATIVE DEFLECTIONS OF
 FLOORS/ROOF DO NOT LOAD/CRUSH
 METAL STUD WALL SYSTEM.

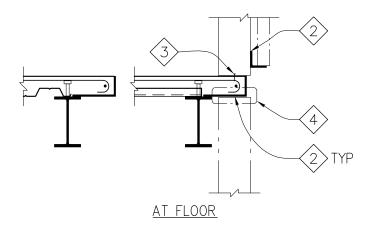
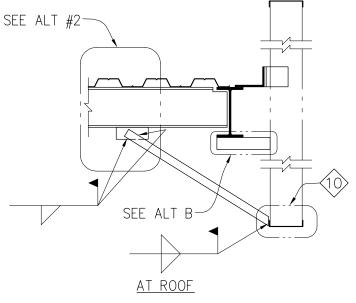


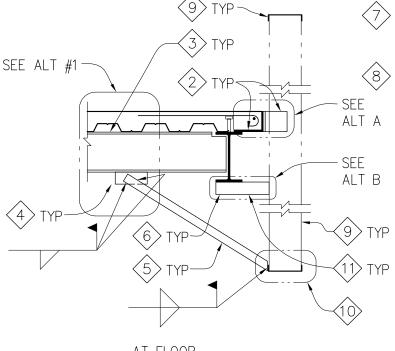


FIGURE 2.2-2 : METAL STUD CONSTRUCTION ISSUES - CASE B: INFILL FRAMING

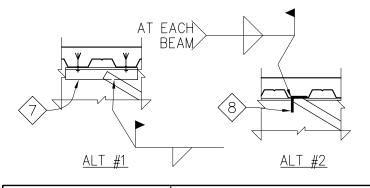


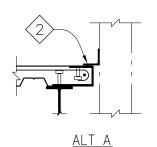


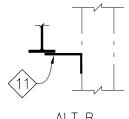
- (1) SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.
- 2 SEE FIGURE 2.2-1 FOR NOTES.
- (3) BEAM.
- 4 PLATE, ANGLE OR WT SHOP WELDED OR BOLTED TO BEAM, 1/4" MINIMUM.
- STUD SUPPLIER) OR ANGLES (SUPPLIED BY STEEL FABRICATOR & INSTALLED BY METAL STUD SUPPLIER) AT BEAMS OR BEAMS & INTERMITTENT LOCATIONS (ALT #1 & ALT #2) BY METAL STUD SUPPLIER.
- 6 METAL STUD (BY METAL SUPPLIER) OR ANGLE (SUPPLIED BY STEEL FABRICTOR & INSTALLED BY METAL STUD SUPPLIER) SUPPORT BRACKET.
- ANGLE, WT, OR BUILT-UP PLATE SECTION ANCHORED INTO SLAB BY STEEL FABRICATOR/ERECTOR.
 - ANGLE OR WT SPANNING FROM BEAM TO BEAM BY STEEL FABRICATOR/ERECTOR.
 - 9 METAL STUD FRAME (BY METAL STUD SUPPLIER) OR CHANNEL/TUBE FRAME BY (STEEL FABRICATOR/ERECTOR) W/ METAL STUD INFILL.
 - VERTICAL SLIP IN THE METAL STUD
 WALL SYSTEM IS REQUIRED TO ENSURE
 THAT RELATIVE DEFLECTIONS OF
 FLOORS/ROOF DO NOT LOAD/CRUSH
 METAL STUD WALL SYSTEM.
 - 11) BRACKETS/CONNECTIONS HERE
 COMPLICATE FIRE-PROOFING & FIRE
 SAFING SEQUENCING. SUPPLIED BY
 STEEL FABRICATOR & INSTALLED BY
 METAL STUD SUPPLIER.









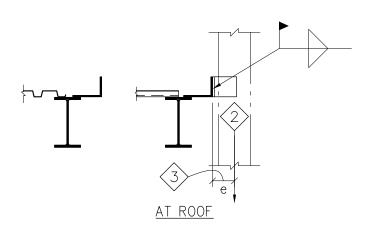


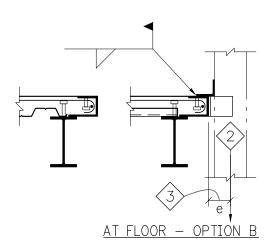
<u>ALT B</u>



FIGURE 2.2-3 : METAL STUD CONSTRUCTION ISSUES - CASE C: STRIP WINDOW PANELS



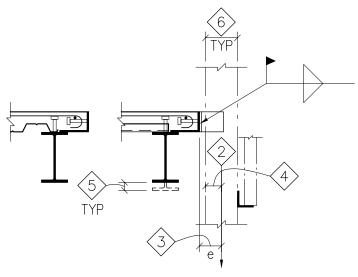






- SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.
- 2 METAL STUD WALL WEIGHT
 (INCLUDING CONNECTIONS, LEDGER
 ANGLES, VENEER, ETC.) AT CENTER OF
 GRAVITY OF METAL STUD WALL SYSTEM.
- TYPICAL ECCENTRICITY 'e' FOR WHICH METAL STUD WALL SYSTEM & CONNECTIONS TO STEEL ARE DESIGNED (NON-VERTICAL SLIP CLIP CONDITION).

 e = ds + dgap + c
 SEE CHART IN FIGURE 2.1b FOR VALUES.
- DISTANCE FROM CENTER OF GRAVITY OF METAL STUD WALL SYSTEM TO INSIDE FACE OF METAL STUD WALL SYSTEM 'c'.
- 5 TYPICAL MAXIMUM LIVE LOAD DEFLECTIONS SHOULD BE LIMITED TO 3/8".
- 6 METAL STUD WALL SYSTEM THICKNESS 't'.

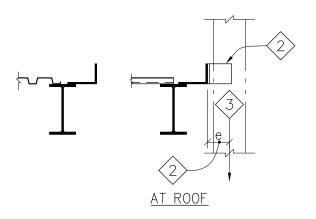


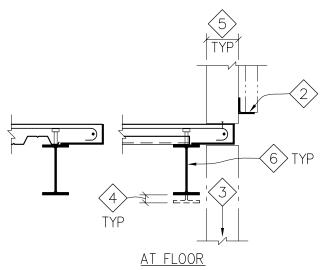
AT FLOOR - OPTION A



FIGURE 2.3-1 : METAL STUD ENGINEERING ISSUES - CASE A: BALLOON FRAMING





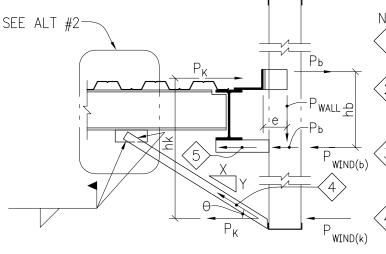


- SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.
- 2 SEE FIGURE 2.3-1 FOR NOTES.
- METAL STUD WALL WEIGHT
 (INCLUDING CONNECTIONS, LEDGER
 ANGLES, VENEER, ETC.) AT CENTER OF
 GRAVITY OF METAL STUD WALL SYSTEM.
- TYPICAL MAXIMUM LIVE LOAD DEFLECTIONS SHOULD BE LIMITED TO 3/8".
- 5 METAL STUD WALL SYSTEM THICKNESS
- 6 FIRE-PROOFING MUST GO ON STEEL PRIOR TO INSTALLING METAL STUD WALL SYSTEM.



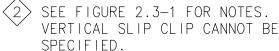
FIGURE 2.3-2 : METAL STUD ENGINEERING ISSUES - CASE B: INFILL FRAMING





AT ROOF

SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.



TYPICAL MAXIMUM LIVE LOAD DEFLECTIONS SHOULD BE LIMITED TO 3/8".

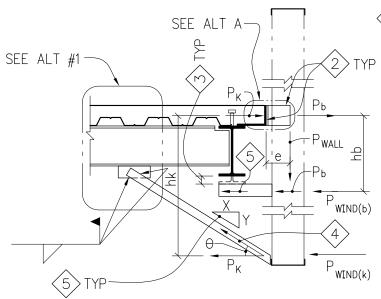
KICKER LOAD:

$$T/C = \frac{[P_k + PWIND(k)]}{COS \Theta}$$

MINIMIZING Y/X REDUCES HORIZONTAL

THRUST INDUCES IN METAL STUD WALL DUE TO BEAM VERTICAL DEFLECTIONS.

WHERE: $P_k = (P_{WALL})(e/hk)$



AT FLOOR

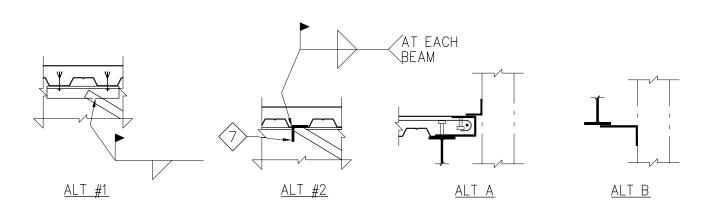
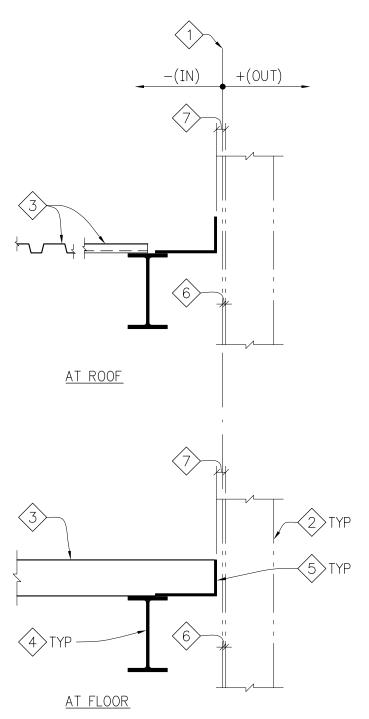




FIGURE 2.3-3 : METAL STUD ENGINEERING
ISSUES - CASE C: STRIP WINDOW
CENTER PANELS

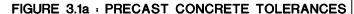




- 1 THEORETICAL INSIDE FACE OF PRECAST CONCRETE SYSTEM.
- 2 PRECAST CONCRETE SYSTEM.
- 3 SLAB/DECK.
- 4 SPANDREL BEAM/GIRDER.
- (5) EDGE ANGLE/BENT PLATE.
- PRECAST CONCRETE SYSTEM ± TOLERANCE. SEE FIGURE 3.1b FOR CHART.
- TEDGE OF SLAB/DECK TO INSIDE FACE OF PRECAST CONCRETE SYSTEM GAP 'dgap' REQUIRED:

 dgap = (ds+) + (dw-).
 SEE FIGURE 3.1b FOR CHART.





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HEIGHT	ds (in)		dw (in)		dgap	e (CASE C)
(ft)	-(IN)	+(OUT)	-(IN)	+(OUT)	(in)	(in)
10	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
20	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
30	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
40	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
50	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
60	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
70	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
80	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
90	0.5	0.5	0.25	0.25	0.75	1.25 + t/2
100	0.5	0.5	0.25	0.25	0.75	1.25 + t/2

NOTES: ds = de (VALUES TAKEN FROM CHART IN FIGURE 1.3b)

dw = EXTERIOR WALL SYSTEM TOLERANCE

dgap = (ds+) + (dw-)

dgap = 0.75" IS COMMON SPECIFIED 'GAP'

e = ds + dgap + t/2

SEE FIGURES 3.3 FOR GRAPHIC DEPICTION OF 'e' & 't'



FIGURE 3.1b : PRECAST CONCRETE TOLERANCES

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1> SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.



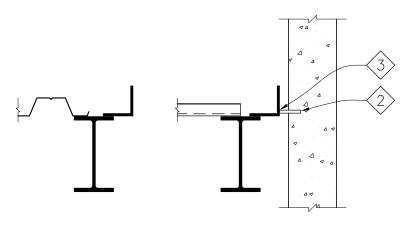
SLOTTED INSERT. INSERT ALLOWS FOR VERTICAL SLIP AND ROTATION OF PRECAST CONCRETE WITH RESPECT TO STEEL FRAMING BY PRECAST CONCRETE SUPPLIER.



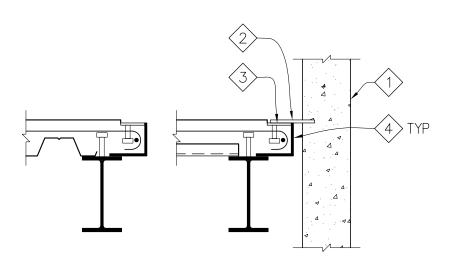
CONNECTION TO STEEL BY PRECAST CONCRETE SUPPLIER.



EDGE ANGLE/BENT PLATE, 1/4" THICK MINIMUM.



AT ROOF

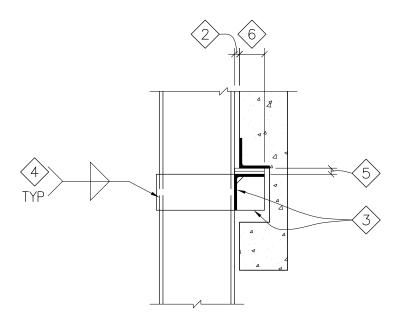


AT FLOOR



FIGURE 3.2-1: PRECAST CONCRETE CONSTRUCTION ISSUES - CASE A





- SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.
- 2 'dgap' REQUIRED = VALUE OBTAINED FROM FIG. 3.1b
- 3 STEEL BRACKET (ANGLES, WT'S, WIDE FLANGES, TUBES, CHANNELS, ETC.) IF INSTALLED IN SHOP, BY STEEL FABRICATOR. IF INSTALLED IN FIELD, BY PRECAST CONCRETE SUPPLIER. TYPICALLY IT IS MORE EFFICIENT & COST EFFECTIVE FOR THE PROJECT TO INSTALL BRACKETS IN THE SHOP.
- 4 CONNECTION IN SHOP (BY STEEL FABRICATOR) OR IN FIELD (BY PRECAST CONCRETE SUPPLIER).
- 5 SHIM STACK FOR FIELD ADJUSTMENT (TYPICALLY 1" THICK) BY PRECAST CONCRETE SUPPLIER. IT IS SIGNIFICANTLY MORE EFFICIENT & COST EFFECTIVE TO PROVIDE A SHIM STACK TO AVOID ELEVATION ERRORS & THUS, COSTLY REPAIRS IN THE FIELD.
- 6 2" MIN BEARING TYPICALLY REQUIRED BY PRECAST CONCRETE SUPPLIER.

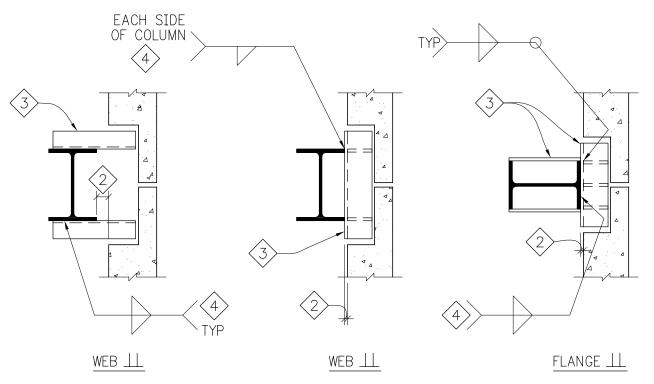




FIGURE 3.2-2a : PRECAST CONCRETE

CONSTRUCTION ISSUES - CASE B

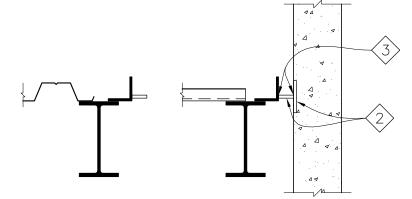




1> SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.



LATERAL SUPPORT FOR PRECAST CONCRETE TYPICALLY AT 4'-0" OC. MATERIAL AND CONNECTIONS BY PRECAST CONCRETE SUPPLIER. INSERT ALLOWS FOR VERTICAL SLIP AND ROTATION OF PRECAST CONCRETE WITH RESPECT TO STEEL FRAMING.



CONNECTION TO STEEL BY PRECAST CONCRETE SUPPLIER.

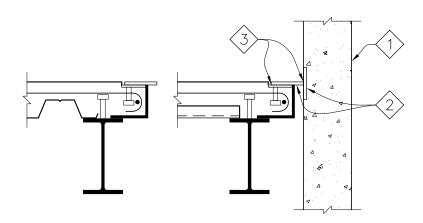


FIGURE 3.2-2b

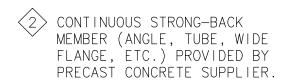


FIGURE 3.2-2b : PRECAST CONCRETE **CONSTRUCTION ISSUES - CASE B**





1) SEE FIGURES 1.4 FOR STEEL FRAMING NOTES.



- WELD FROM PRECAST CONCRETE TO STRONG-BACK TO STEEL FRAMING BY PRECAST CONCRETE SUPPLIER.
- 4 EMBED PLATE BY PRECAST CONCRETE SUPPLIER.
 TYPICALLY SUPPORTS FOR WEIGHT OF PRECAST CONCRETE ARE PROVIDED AT 2 LOCATIONS NEAR THE ENDS OF THE STEEL SPANDREL BEAM/GIRDER.

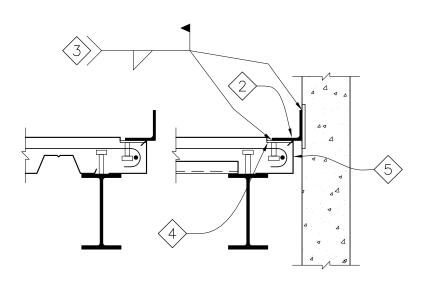
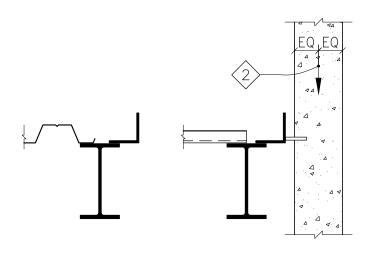




FIGURE 3.2-3 : PRECAST CONCRETE

CONSTRUCTION ISSUES - CASE C







- SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.
- 2 PRECAST CONCRETE WALL WEIGHT CARRIED BY BUILDING FOUNDATION.
- 3 PRECAST CONCRETE THICKNESS 't'.

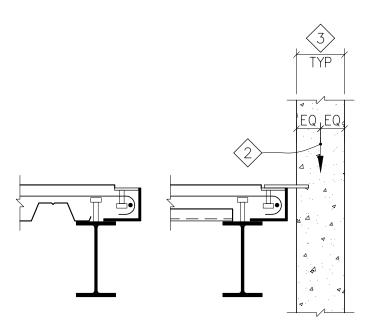
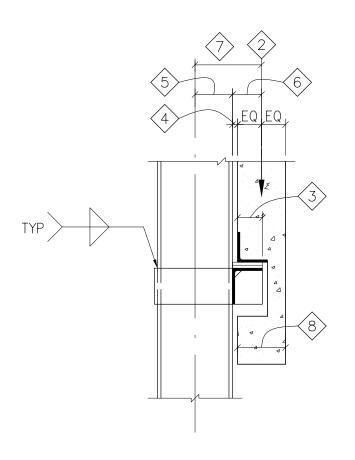




FIGURE 3.3-1 : PRECAST CONCRETE ENGINEERING ISSUES - CASE A





- 1) SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.
- 2 PRECAST CONCRETE WALL WEIGHT.
- 3 2" MINIMUM BEARING.
- 4 PRECAST CONCRETE WALL TO STEEL COLUMN FACE SPACE 'dp'.
- 5 STEEL COLUMN WIDTH/2 'dcol/2'.
- TYPICAL ECCENTRICITY 'e' FOR WHICH BRACKET & CONNECTION STEEL COLUMN ARE DESIGNED FOR:

$$e = t/2 + dp$$

- 7 TYPICAL ECCENTRICITY FOR WHICH THE COLUMN IS DESIGNED FOR:
 e = t/2 + dp + dcol/2
- 8> PRECAST CONCRETE THICKNESS 't'.

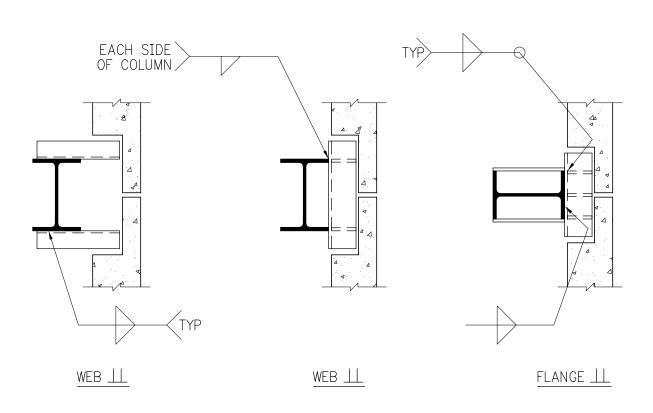




FIGURE 3.3-2a : PRECAST CONCRETE ENGINEERING ISSUES - CASE B



EQ EQ 3

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NOTES:

- 1) SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.
- 2 LATERAL FORCE DUE TO WIND AND REQUIREMENTS FOR LATERALLY BRACING THE PRECAST CONCRETE FOR GRAVITY LOADS.
- PRECAST CONCRETE WALL WEIGHT CARRIED BY STEEL COLUMNS.

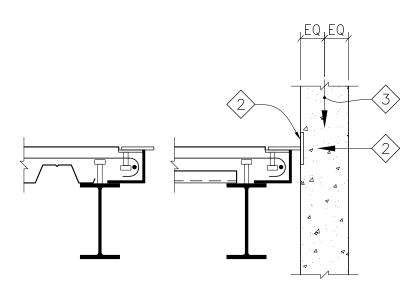




FIGURE 3.3-2b : PRECAST CONCRETE
ENGINEERING ISSUES - CASE B





(1) SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.



PRECAST CONCRETE WALL WEIGHT.



TYPICAL ECCENTRICITY 'e' FOR WHICH CONTINUOUS STRONG-BACK MEMBER TO STEEL & CONNECTIONS ARE DESIGNED FOR: e = ds + dgap + t/2

SEE CHART IN FIGURE 3.16 FOR VALUES.



(4) PRECAST CONCRETE THICKNESS 't'.

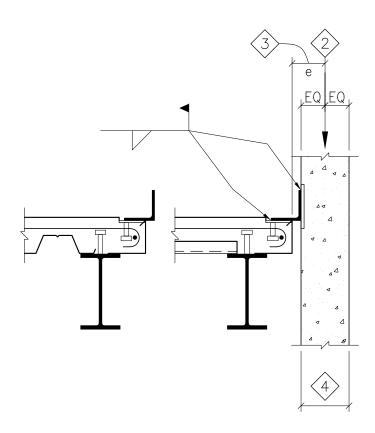
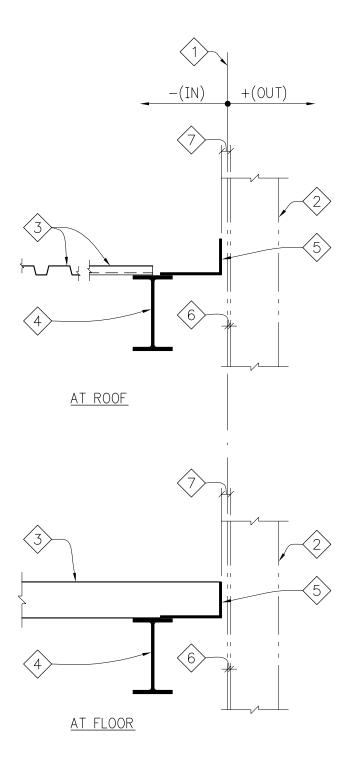




FIGURE 3.3-3 : PRECAST CONCRETE **ENGINEERING ISSUES - CASE C**





- 1 THEORETICAL INSIDE FACE OF CURTAIN WALL SYSTEM.
- 2 CURTAIN WALL SYSTEM.
- \$\langle 3 \rangle SLAB/DECK.
- 4 SPANDREL BEAM/GIRDER.
- (5) EDGE ANGLE/BENT PLATE.
- 6 CURTAIN WALL SYSTEM ± TOLERANCE. SEE FIGURE 4.1b FOR CHART.
- TEDGE OF SLAB/DECK TO INSIDE FACE OF CURTAIN WALL SYSTEM GAP 'dgap' REQUIRED:

 dgap = (ds+) + (dw-)
 SEE FIGURE 4.1-1b FOR CHART.







HEIGHT	ds (in)		dw (in)		dgap	е	
(in)	-(IN)	+(OUT)	-(IN)	+(OUT)	(in)	(in)	
10	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
20	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
30	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
40	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
50	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
60	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
70	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
80	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
90	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	
100	0.5	0.5	0.06	0.06	0.56	1.25 + t/2	

NOTES: ds = de (VALUES TAKEN FROM CHART IN FIGURE 1.3b)

dw = EXTERIOR WALL SYSTEM TOLERANCE

dgap = (ds+) + (dw-)

dgap = 0.75" IS A COMMON SPECIFIED 'GAP'

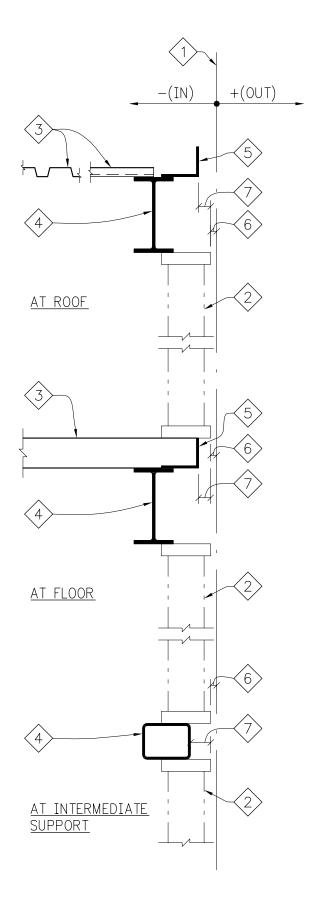
e = ds + dgap + t/2

SEE FIGURE 4.3-1 FOR GRAPHIC DEPICTION OF 'e' & 't'



FIGURE 4.1-1b : CURTAIN WALL TOLERANCES

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- 1) THEORETICAL INSIDE FACE OF STOREFRONT SYSTEM.
- 2 STOREFRONT SYSTEM.
- 3 SLAB/DECK.
- 4 SPANDREL BEAM/GIRDER/GIRT.
- (5) EDGE ANGLE/BENT PLATE.
- 6 STOREFRONT SYSTEM
 ± TOLERANCE. SEE FIGURE 4.1-2b
 FOR CHART.
- The state of the s

dgap = ds(OUT) + dw(IN).



FIGURE 4.1-2a : STOREFRONT TOLERANCES



HEIGHT	ds (in)		dw (in)		dgap	е
(in)	-(IN)	+(OUT)	-(IN)	+(OUT)	(in)	(in)
10	0.5	0.5	0.06	0.06	0.56	N/A
20	0.5	0.5	0.06	0.06	0.56	N/A
30	0.5	0.5	0.06	0.06	0.56	N/A
40	0.5	0.5	0.06	0.06	0.56	N/A
50	0.5	0.5	0.06	0.06	0.56	N/A
60	0.5	0.5	0.06	0.06	0.56	N/A
70	0.5	0.5	0.06	0.06	0.56	N/A
80	0.5	0.5	0.06	0.06	0.56	N/A
90	0.5	0.5	0.06	0.06	0.56	N/A
100	0.5	0.5	0.06	0.06	0.56	N/A

NOTES: ds = de (VALUES TAKEN FROM CHART IN FIGURE 1.3b)

dw = EXTERIOR WALL SYSTEM TOLERANCE

dgap = (ds+) + (dw-)

dgap = 0.75" IS A COMMON SPECIFIED 'GAP'

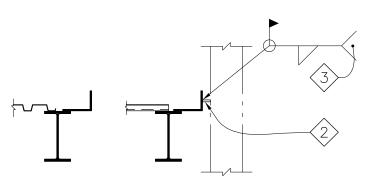
SEE FIGURE 4.3-1 FOR GRAPHIC DEPICTION OF 'e'



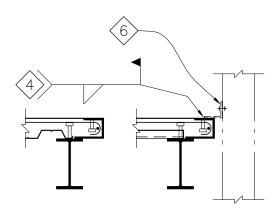
FIGURE 4.1-2b : STOREFRONT TOLERANCES

DISCA

ROCKY MOUNTAIN STEEL CONSTRUCTION ASSOCIATION



AT ROOF



AT FLOOR - OPTION B



- SEE FIGURE 1.4 FOR STEEL FRAMING NOTES.
- TYPICALLY 1/4" OR 3/8" DIAMETER
 (1/2" DIAMETER ANCHORS ARE USED
 FOR UNCONVENTIONAL/HEAVY SYSTEMS)
 CURTAIN WALL ANCHORS (BY CURTAIN
 WALL SUPPLIER), ANCHORED TO
 MID-HEIGHT OF EDGE ANGLE/
 BENT PLATE.
- ANCHORS ARE FIELD WELDED BY
 CURTAIN WALL SUPPLIER TO THE
 VERTICAL FACE OF THE EDGE ANGLE/
 BENT PLATE AT EACH MULLION (WELD
 IS BY CURTAIN WALL SUPPLIER).
- 4 FIELD WELD/ANCHOR/SCREW BY CURTAIN WALL SUPPLIER.
- 5 EDGE ANGLE/BENT PLATE, 1/4" THICK MINIMUM.
- 6 ANGLE OR PLATE & ATTACHMENT TO CURTAIN WALL BY CURTAIN WALL SUPPLIER.

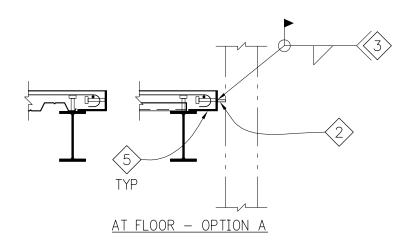
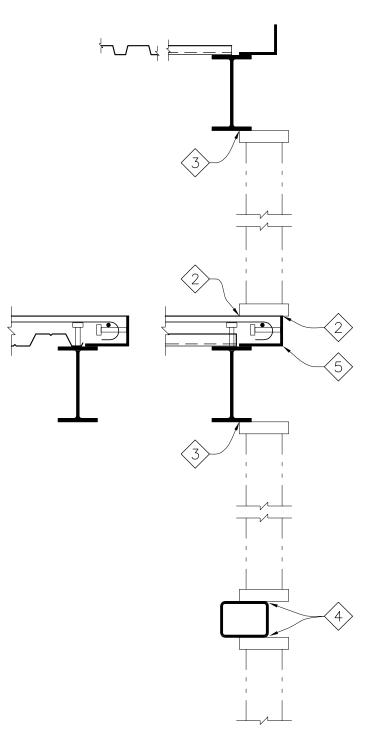




FIGURE 4.2-1 : CURTAIN WALL CONSTRUCTION ISSUES



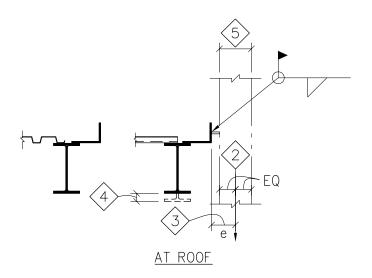


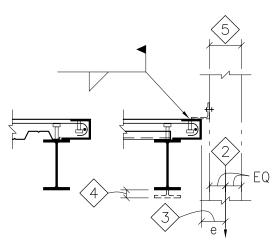
- SEE FIGURE 1.4 FOR STEEL FRAMING NOTES.
- CONNECTION TO EDGE ANGLE/BENT PLATE VIA WELDS, CLIPS, ETC.
 CONNECTION TO SLAB VIA EXPANSION ANCHORS, WELD TO EMBED PLATES, ETC.
 BY STOREFRONT SUPPLIER.
- CONNECTION TO BEAMS/GIRDERS VIA CLIPS THAT ALLOW VERTICAL SLIP TO ACCOUNT FOR ROOF/FLOOR LIVE LOAD DEFLECTIONS BY STOREFRONT SUPPLIER.
- 4 CONNECTION TO GIRTS VIA CLIPS, WELDS, ETC. BY STOREFRONT SUPPLIER.
- 5 EDGE ANGLE/BENT PLATE, 1/4"
 MINIMUM.



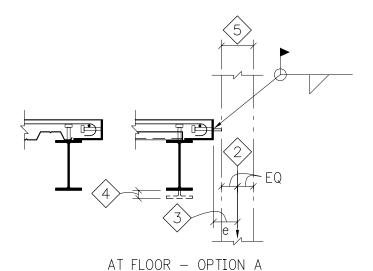








<u>AT FLOOR - OPTION B</u>



- SEE FIGURE 1.5 FOR STEEL FRAMING NOTES.
- 2 CURTAIN WALL SYSTEM WEIGHT (INCLUDING CONNECTIONS).
- TYPICALLY ECCENTRICITY 'e' FOR WHICH CURTAIN WALL FRAMING & CONNECTIONS TO STEEL ARE DESIGNED FOR:

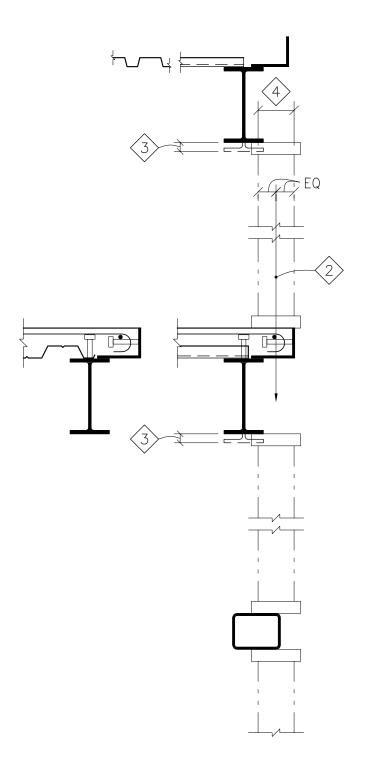
 e = ds + dgap + t/2.

 SEE CHART IN FIGURE 4.1-1b FOR VALUES.
- TYPICAL MAXIMUM LIVE LOAD DEFLECTIONS SHOULD BE LIMITED TO 1/4".
- (5) CURTAIN WALL THICKNESS 't'.



FIGURE 4.3-1: CURTAIN WALL ENGINEERING ISSUES





- SEE FIGURES 1.5 FOR STEEL FRAMING NOTES.
- \$\leq 2 \ STOREFRONT SYSTEM WEIGHT
 (INCLUDING CONNECTIONS).
- TYPICAL MAXIMUM LIVE LOAD DEFLECTIONS SHOULD BE LIMITED TO 1/4".
- 4 STOREFRONT THICKNESS 't'.



FIGURE 4.3-2 : STOREFRONT ENGINEERING ISSUES

